

Three phase circuits

Modern power system transmits three phase-shifted sinusoidal currents through three parallel wires across long distances.

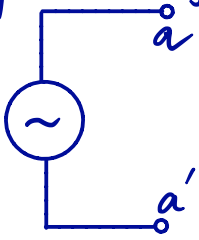
From these three-phase (denoted 3ϕ) circuits, often a single phase supplies your home.

However, in this course, we will only deal with 3ϕ generators supplying power to 3ϕ loads only.

Why 3ϕ ? Why not 1ϕ , 2ϕ , 4ϕ , etc.?

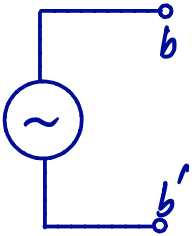
Three phase power generation has advantages that we will cover later in the course.

To explain 3 ϕ circuits, consider 3 sinusoidal voltage sources that are phase-shifted by 120 degrees as follows.



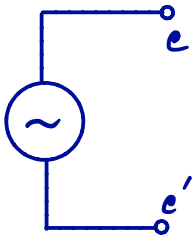
$$v_{aa'}(t) = v_o \cos(\omega t + \theta_v)$$

$$\bar{V}_{aa'} = \frac{v_o}{\sqrt{2}} \angle \theta_v$$



$$v_{bb'}(t) = v_o \cos(\omega t + \theta_v - 120^\circ)$$

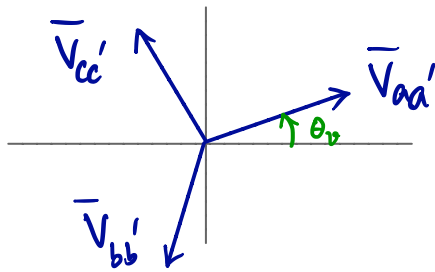
$$\bar{V}_{bb'} = \frac{v_o}{\sqrt{2}} \angle (\theta_v - 120^\circ)$$

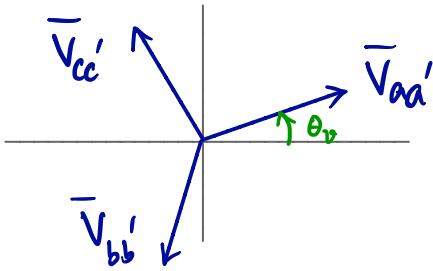


$$v_{cc'}(t) = v_o \cos(\omega t + \theta_v + 120^\circ)$$

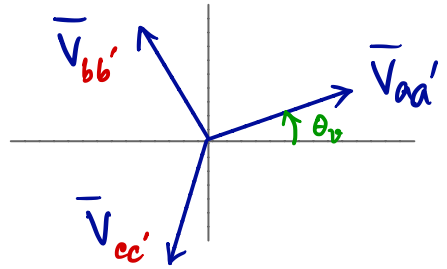
$$\bar{V}_{cc'} = \frac{v_o}{\sqrt{2}} \angle (\theta_v + 120^\circ)$$

Phasor
diagram :





Such a sequence is called a positive (+ve) sequence.

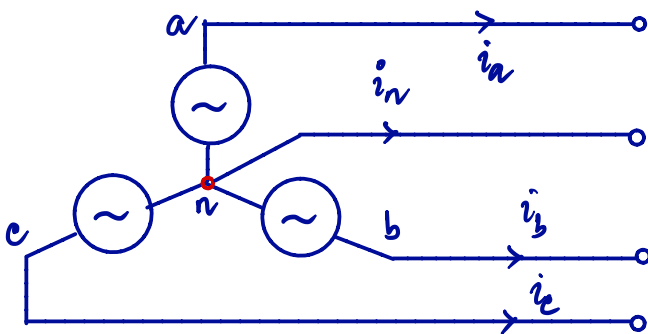


Such a sequence is called a negative (-ve) sequence.

Claim: $\bar{V}_{aa'} + \bar{V}_{bb'} + \bar{V}_{cc'} = 0$.

Verify it with elementary complex arithmetic.

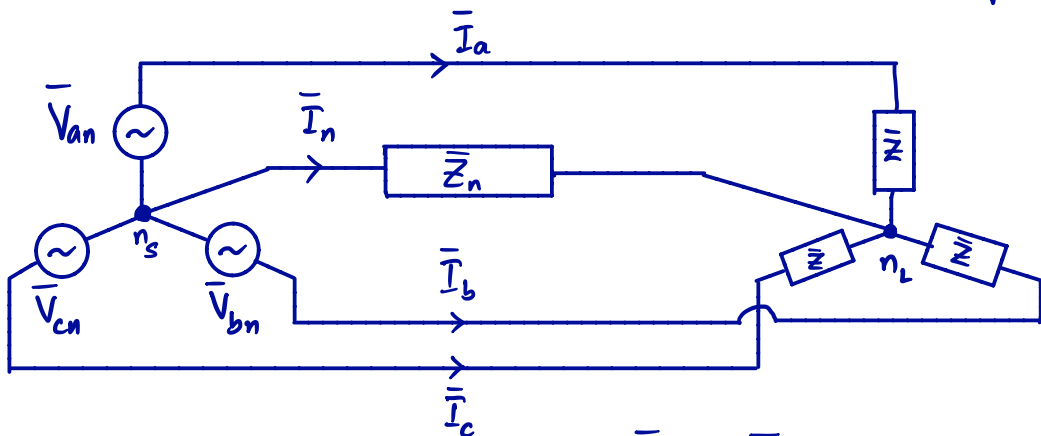
Let us interconnect a' , b' , c' terminals.



Terminal "n" is called neutral.

This interconnection is a "WYE" connected source.

Let us interconnect this "ye" connected source to a "ye" connected load as follows



• Claim 1: $\bar{I}_n = 0$, and $\bar{V}_{n_s} - \bar{V}_{n_l} = 0$.

Proof: $\bar{V}_{an} - \bar{I}_a \bar{Z} + \bar{I}_n \bar{Z}_n = 0$.

$$\bar{V}_{bn} - \bar{I}_b \bar{Z} + \bar{I}_n \bar{Z}_n = 0.$$

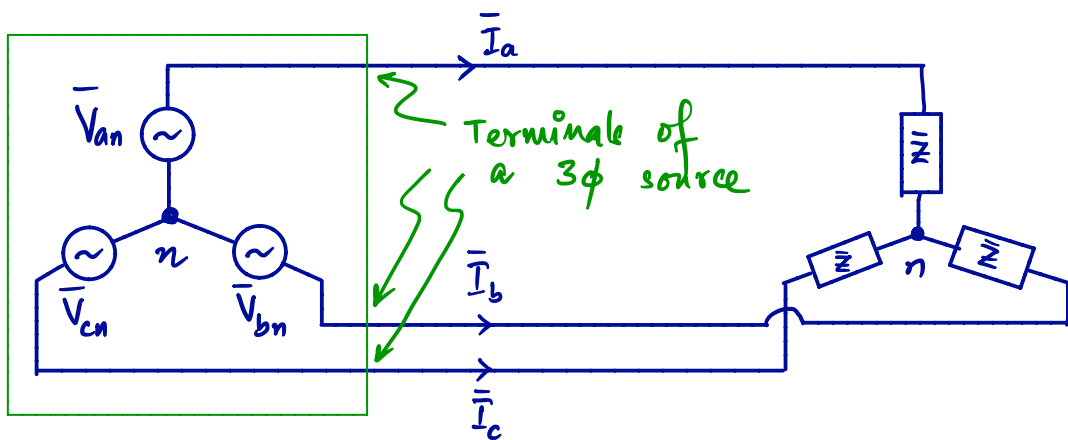
$$\bar{V}_{cn} - \bar{I}_c \bar{Z} + \bar{I}_n \bar{Z}_n = 0$$

Add them together.

$$0 - \underbrace{(\bar{I}_a + \bar{I}_b + \bar{I}_c)}_{= -\bar{I}_n \text{ by Kirchhoff's current law}} \bar{Z} + 3\bar{I}_n \bar{Z}_n = 0.$$

$$\Rightarrow \bar{I}_n (3\bar{Z}_n + \bar{Z}) = 0 \Rightarrow \bar{I}_n = 0 \text{ (why?).}$$

In this course, we will only consider "balanced" loads, i.e., each branch or phase of the load is identical. For balanced 3 ϕ sources & loads, $\bar{I}_n = 0$
 \Rightarrow we can ignore the line interconnecting the neutral terminals.



Definition: The magnitude of voltage differences across the branches or phases of a 3 ϕ -component is called **phase voltage**.

$$V_{\phi} = |\bar{V}_{an}| = |\bar{V}_{bn}| = |\bar{V}_{cn}|.$$

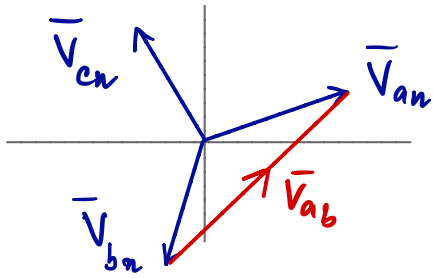
Definition: Magnitude of voltage differences between the terminals of a 3 ϕ -component is called **line-to-line** or **line** voltage.

$$V_L = |\bar{V}_{ab}| = |\bar{V}_{bc}| = |\bar{V}_{cn}|.$$

• Claim: $V_L = \sqrt{3} V_\phi$.

Proof:

$$\begin{aligned} V_L &= |\bar{V}_{ab}| \\ &= |\bar{V}_{an} - \bar{V}_{bn}| \\ &= \left| \frac{V_0}{\sqrt{2}} \angle \theta_v - \frac{V_0}{\sqrt{2}} \angle (\theta_v - 120^\circ) \right| \\ &= \left| \frac{V_0}{\sqrt{2}} \angle \theta_v (1 - e^{j\omega(-120^\circ)}) \right| \\ &= \frac{V_0}{\sqrt{2}} \cdot \left| 1 - \left(-\frac{1}{2} - j\frac{\sqrt{3}}{2}\right) \right| \\ &= V_\phi \left| \frac{3}{2} + j\frac{\sqrt{3}}{2} \right| = \sqrt{3} \cdot V_\phi. \end{aligned}$$

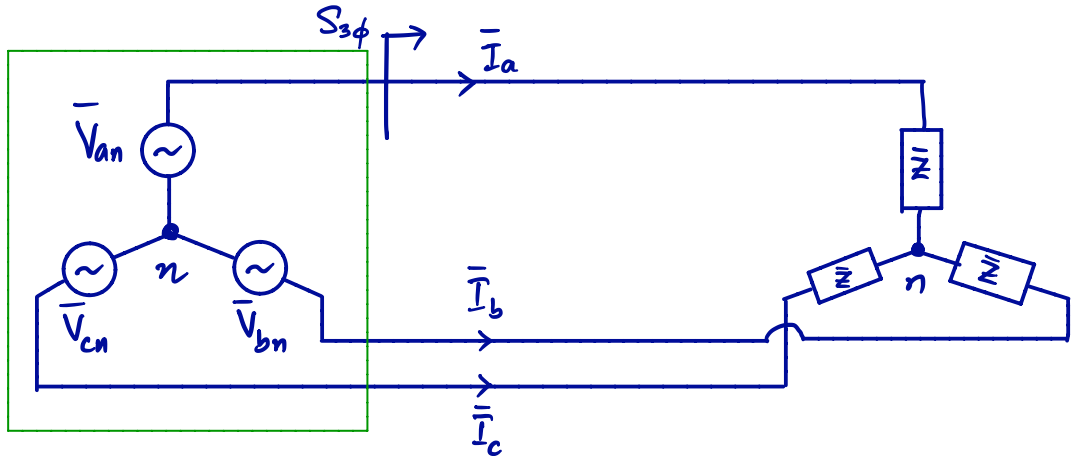


Phasor diagram showing phase and line voltage phasors.

Definition: Current magnitude on each branch of a 3 ϕ component is called **phase** current. And, current magnitude flowing at the terminal is called **line** current.

For the wye-connected source, phase current (\bar{I}_ϕ) equals line current (I_L), given by $|\bar{I}_a|$, i.e.,

$$I_\phi = I_L = |\bar{I}_a| = |\bar{I}_b| = |\bar{I}_c|.$$



• Claim: The 3 ϕ complex power is given by $S_{3\phi} = \sqrt{3} V_L I_L \angle \theta$, where θ is the angle between \bar{V}_{an} & \bar{I}_a .

Proof:

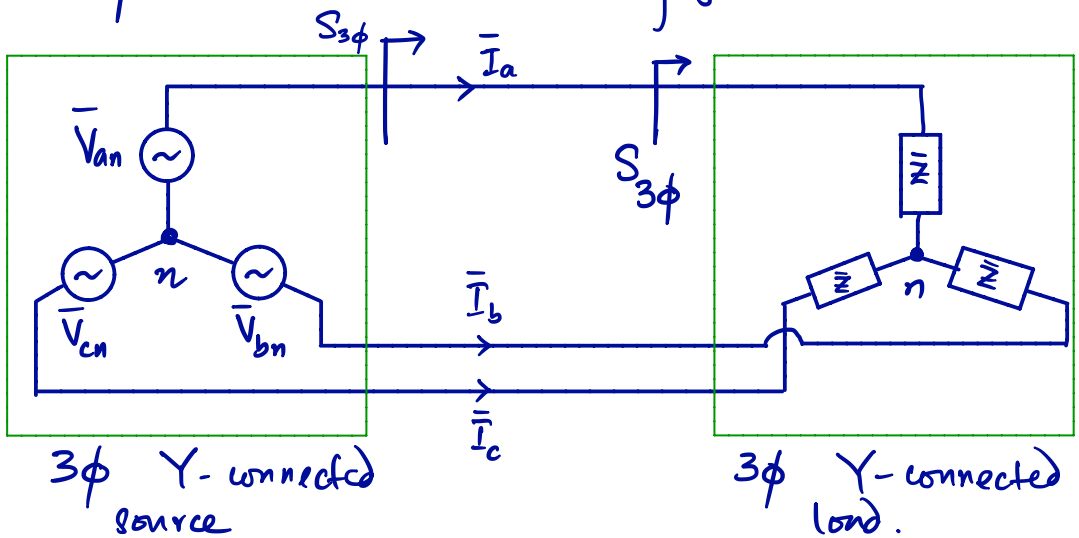
$$S_{3\phi} = \bar{V}_{an} \bar{I}_a^* + \bar{V}_{bn} \bar{I}_b^* + \bar{V}_{cn} \bar{I}_c^*.$$

Recall that phases b and c are phase shifted from a by -120° and $+120^\circ$, respectively.

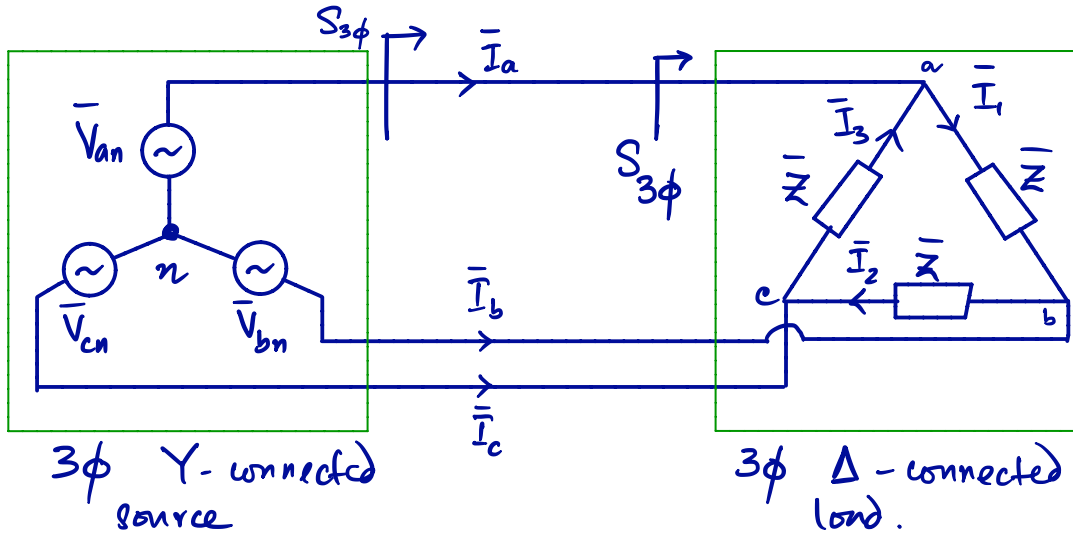
$$\Rightarrow S_{3\phi} = \bar{V}_{an} \bar{I}_a^* + \left(\bar{V}_{bn} \angle -120^\circ \right) \left(\bar{I}_a \angle -120^\circ \right)^* + \left(\bar{V}_{an} \angle +120^\circ \right) \left(\bar{I}_a \angle +120^\circ \right)^*$$

$$\begin{aligned}
 &= 3 \bar{V}_{an} \bar{I}_a^* \\
 &= 3 \left(|\bar{V}_{an}| \angle \bar{V}_{an} \right) \cdot \left(|\bar{I}_a| \angle (-\bar{I}_a) \right) \\
 &= 3 \cdot |\bar{V}_{an}| \cdot |\bar{I}_a| \angle (\bar{V}_{an} - \bar{I}_a) \\
 &= 3 V_\phi I_L \angle \theta \\
 &= \sqrt{3} \cdot V_L I_L \angle \theta
 \end{aligned}$$

$$\therefore \begin{cases} P_{3\phi} = \sqrt{3} V_L I_L \cos \theta \\ Q_{3\phi} = \sqrt{3} V_L I_L \sin \theta \end{cases} \left\{ \begin{array}{l} 3\phi \text{ real and} \\ \text{reactive powers} \\ \text{generated.} \end{array} \right.$$



Wye-connected (Y -connected) source
 & delta-connected (Δ -connected) load.



For the Δ -connected load,

phase voltage $V_\phi = |\bar{V}_{ab}| = |\bar{V}_{bc}| = |\bar{V}_{ca}|$.

phase current $I_\phi = |\bar{I}_1| = |\bar{I}_2| = |\bar{I}_3|$.

line voltage $V_L = |\bar{V}_{ab}| = |\bar{V}_{bc}| = |\bar{V}_{ca}|$

line current $I_L = |\bar{I}_a| = |\bar{I}_b| = |\bar{I}_c|$.

$$\left. \begin{aligned} \bar{I}_a &= \bar{I}_1 - \bar{I}_3, \\ \bar{I}_b &= \bar{I}_2 - \bar{I}_1, \\ \bar{I}_c &= \bar{I}_3 - \bar{I}_2. \end{aligned} \right\} \text{From Kirchhoff's current law.}$$

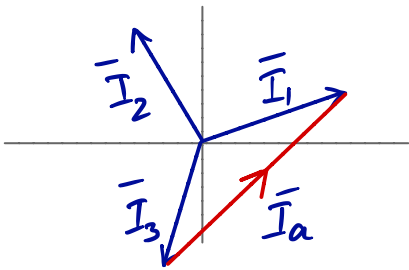
By symmetry, $\bar{I}_1, \bar{I}_2, \bar{I}_3$ are phasors with equal magnitudes, but phase-shifted by 120° .

$$|\bar{I}_1| = |\bar{I}_2| = |\bar{I}_3|,$$

$$\text{and } |\bar{I}_a| = \sqrt{3} |\bar{I}_1|.$$

$$\Rightarrow I_L = \sqrt{3} I_\phi.$$

$$\text{Also, } V_L = V_\phi.$$



Claim: The 3 ϕ complex power delivered to the Δ -connected load is given by

$S_{3\phi} = \sqrt{3} V_L I_L \cos \theta$, where θ is the angle between line voltages & currents, or phase voltages & currents.

$$\bar{V}_{ab} = \bar{Z} \bar{I}_1, \bar{V}_{bc} = \bar{Z} \bar{I}_2, \bar{V}_{ca} = \bar{Z} \bar{I}_3,$$

where $\bar{Z} = |\bar{Z}| \angle \theta$.

Recall that

$$\begin{aligned} S_{3\phi} &= 3 \cdot |\bar{V}_{an}| \cdot |\bar{I}_a| \angle (\bar{V}_{an} - \bar{I}_a) \\ &= \sqrt{3} \cdot |\bar{V}_{ab}| \cdot |\bar{I}_a| \angle \theta \\ &= \sqrt{3} V_L \cdot I_L \angle \theta, \end{aligned}$$

the same as a Y-connected source with a Δ -connected load.

Summary of relationships:

Y-Component	Δ -Component
$V_L = \sqrt{3} V_\phi$	$V_L = V_\phi,$
$I_L = I_\phi$	$I_L = \sqrt{3} I_\phi,$
$S_{3\phi} = \sqrt{3} V_L I_L \angle \theta$	$S_{3\phi} = \sqrt{3} V_L I_L \angle \theta$